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### Hydrogen Gas Incidents

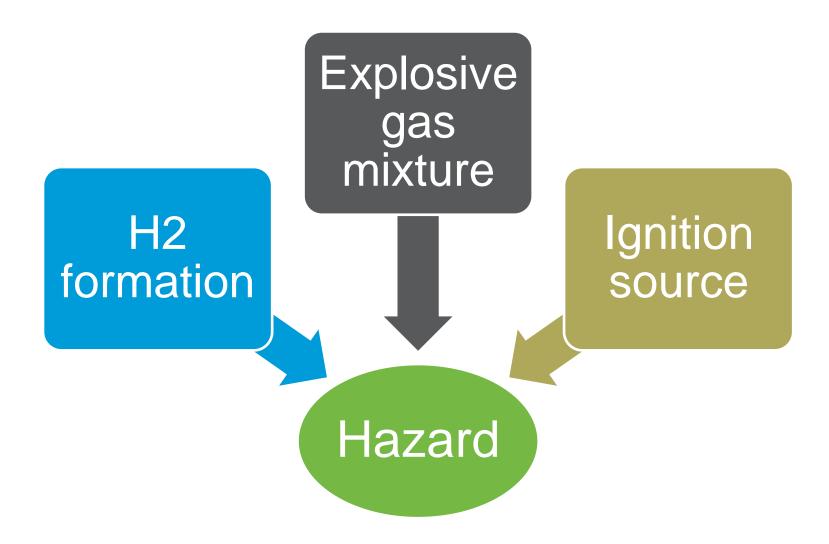
Hannes Storch
Paris, 5th of November 2014

### Agenda

- Theoretical considerations
  - Hazard formation
  - Physical properties of H2/Air mixtures
- Case Study
- Considerations



#### Hazard formation





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#### **Explosion limits**

 Explosion Limits of hydrogen in air and air/nitrogen at room temperature, measured by various standards (in mole-%)

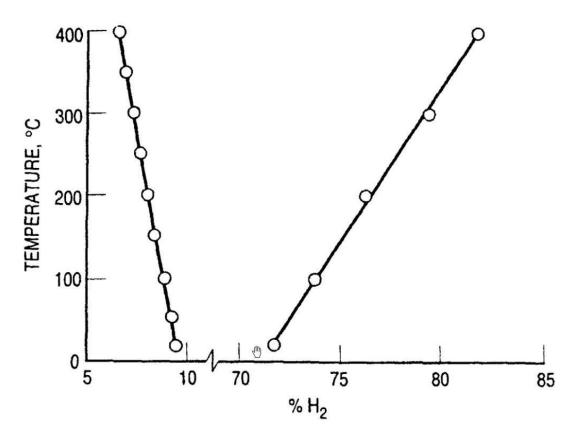
	DIN 51649	EN 1839(T)	EN 1839(B)	ASTM E681
LEL (H <sub>2</sub> in air)	3.8	3.6	4.2	3.75
UEL (H <sub>2</sub> in air)	75.8	76.6	77.0	75.1
LEL (40% N <sub>2</sub> +air)	3.6	3.6	4.4	3.65
UEL (40% N <sub>2</sub> + air)	38.2	38.4	38.2	37.3

- 2<sup>nd</sup> case residual oxygen content is approx. 13%-vol. (~ double the content at the intermediate absorber)
- UEL in this case will be below the tabled figures as the addition of increasing chemically inert substances to mixtures of hydrogen and air causes the upper and lower limits of explosion to approach each other, and ultimately to met.

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#### Influence of gas temperature

 Explosion range of hydrogen – air mixtures widens with increased temperature, which is important at our prevailing conditions

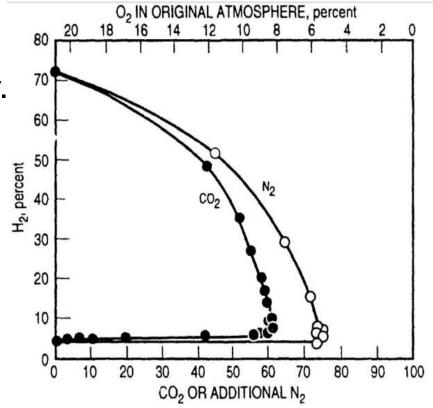




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#### Influence of additional N2 or CO2

- The presence of additional N<sub>2</sub> or CO<sub>2</sub> in the gas (air) will reduce the oxygen content.
- Subject to the residual O<sub>2</sub>, the explosion limits vary significantly.
- No critical compositions at O<sub>2</sub> contents below 4...5%

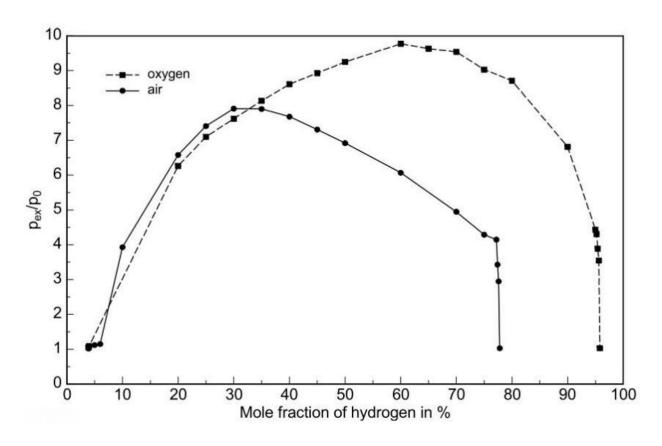




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#### Reaction energy

 $2 H_2 + O_2 = 2 H_2O \rightarrow \Delta H = -483 \text{ kJ/mol}$ High pressure generation due to explosion

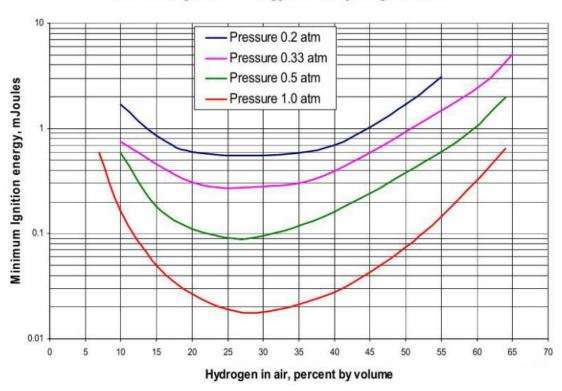




### Required ignition energy

Very small input of energy required for ignition: only 0.02
 mJ at 30 % H2 in air

#### Minimum Ignition Energy vs. % Hydrogen in Air



#### H<sub>2</sub> generation – an example

- Scenario: Catastrophic corrosion of a 1000 m² heat exchanger:
- Assumption:
  - Acid (100C, 80%) leads to a corrosion rate of 10 mm/y
  - Amount of H<sub>2</sub> after 1 hour : approx. 9 kg (or 100 Nm<sup>3</sup>)
- Volume of IP tower top ~ 700 m³ (or less if only "dead" volume is considered on top of exit, say 150m³)
- H<sub>2</sub> concentration after one hour is between 15 and 65 vol-%, which is well within explosion limits (UEL reached after 5 – 20 minutes)

After a short period after re-commissioning of Plant an Hydrogen-Explosion occured, this event was originated by *acid cooler leak in closed loop system.* 

Reason for leak could be: tube sheet failure, tube leak from acid/water side, maintenance, anodic protection, etc.





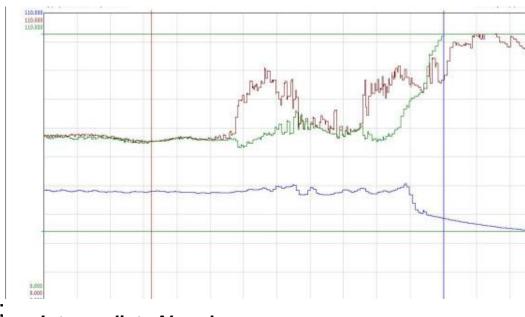


#### What has happened?

Plant operated at partial load.

At a certain time high temperature in cooling water loop was realized, but communication failed.

- + 1:30 First local samples were taken
- + 2:05 Confirmation of result and shut-down initiated
- + 2:30 Acid concentration below 91%; CW pressure > Acid pressure
  - → Cooling water stopped
  - → Acid circulation and blower



## Intermediate Absorber Cooling water temperature, out: red (cooler 1) green (cooler 2)

stopped

+ 3:00 First explosion

Less than 30 minutes between stop of blower and explosion!!



blue (main blower)

#### Have there been Warnings?

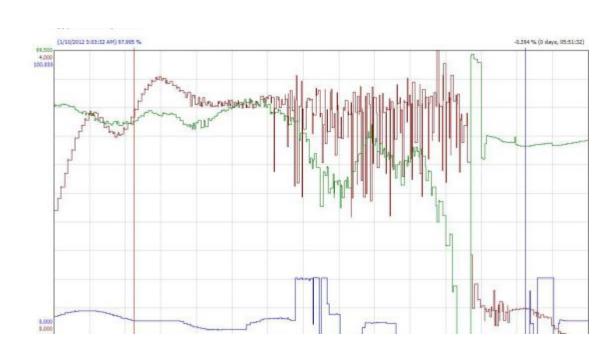
Cooling water temperatures

Pressure of cooling water in closed loop system (red)

Acid concentration (grün)

Dilution water (blue)

Anodic protection system (n.a.)



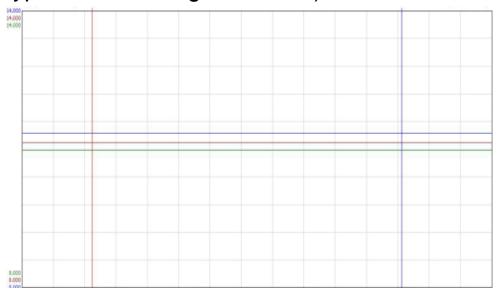
Instabilites in trend are good indication of up-set conditions!!



#### Why was the leak detected so late?

Each cooler is monitored by a pH-measurement.

No alarms during operation (!) ....... as probes have not been re-installed (in other cases instruments bypassed, alarm ignored, etc.)





Static trends can tell something too!!



#### What else supported the incident?

Closed loop cooling water systems have pressure levelling device to maintain cooling water pressure < acid pressure.

If this is not in operation; reaction in cooler a far more violent as water enters into acid.

Closed loop systems have typically smaller water inventory, which support formation of weak acid.

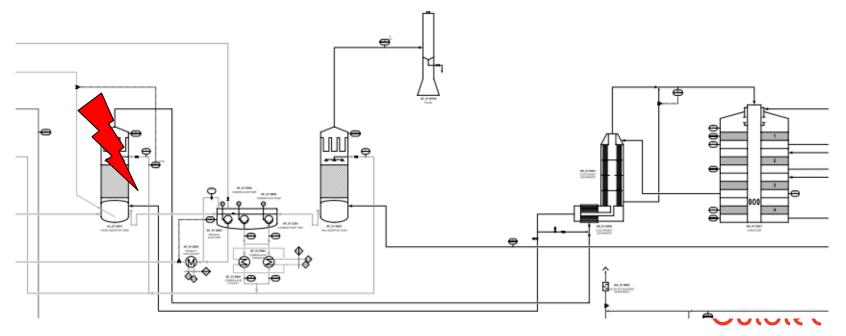




#### Which equipment was affected?

Damage must be expected by (I) weak acid, (II) explosion, (III) repair time

- (I) Cooling water system, acid piping system, acid cooler, acid pumps, irrigation, system
- (II) IAT (Candle filters, dome, packing), Cold Re-heat exchanger, Converter, Blower, (T/G-set)
- (III) Acid piping, irrigation systems, catalyst etc.



#### Which equipment was effected?

Acid coolers: Completly

damaged





Acid Piping: Circulation was stopped early, no damage

Pump tank: No damage in bricklined tank (despite the fact, that acid of 85% was stored for extended time)

Acid Pumps: Removed imediately, no damage



Which equipment was affected?

Intermediate Absober

Candle Filters: Destroyed

**Tube Sheet: Deformed** 

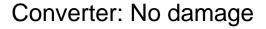
Packing: Contaminated by fibers

Dome and brickwork: No Damage

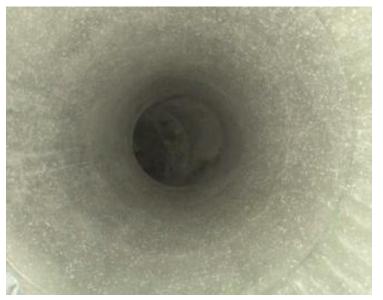


#### Which equipment was affected?

Heat Exchanger: Baffles damaged



Blower: No damage







#### Conclusion

#### What can we learn .....

.... Hydrogen formation can be extremly fast under certain conditions. Due to the wide explosion range and low explosion energy the risk of hazardous situation is high.

..... A failure in an acid cooler (or boiler, economizer etc) can and will happen.

...... An early detection and fast isolation can help to avoid hydrogen explosions

...... Good operation and maintenance practice is fundamental (Interpret process data)

..... Consider infrastructure in adequate way



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